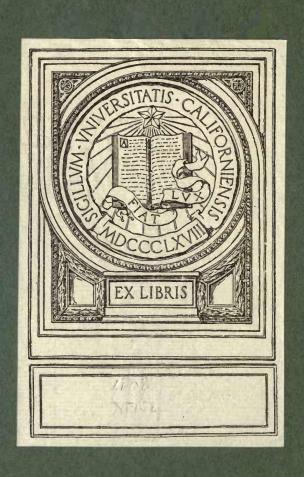
T H 2398 M3



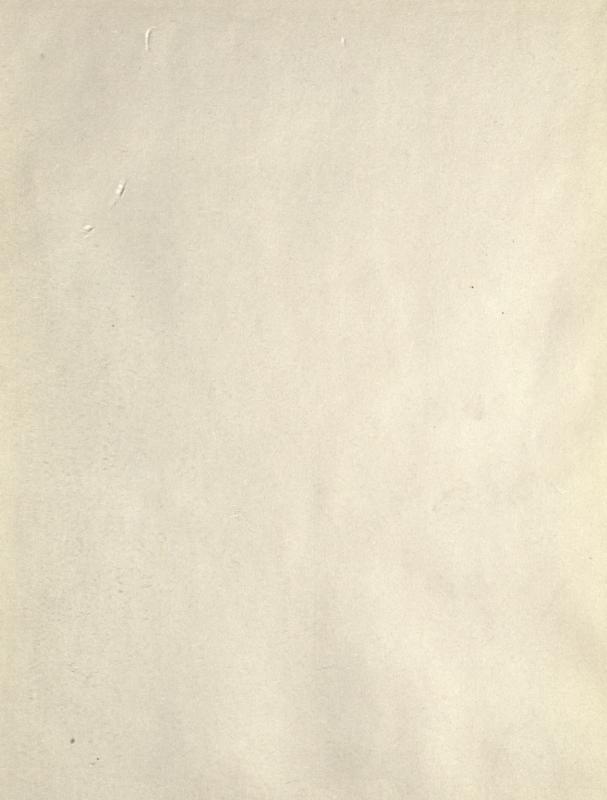
HIP AND VALLEY DESIGN

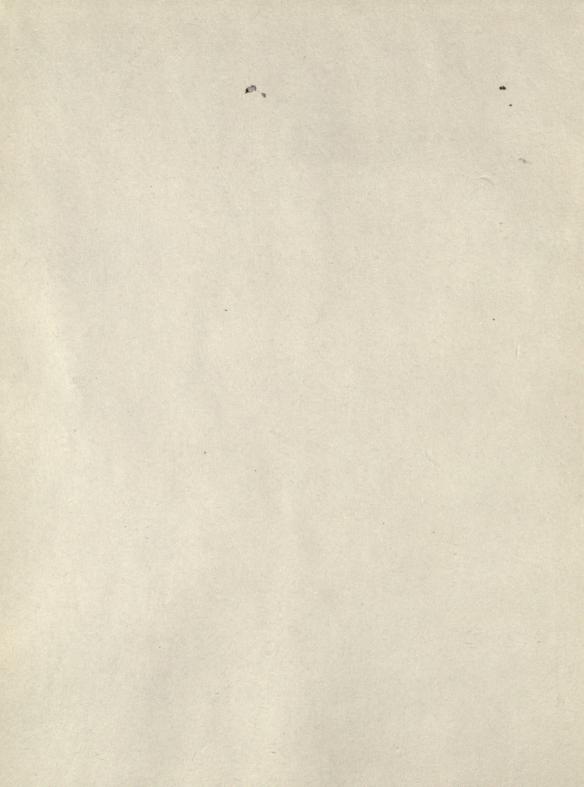
DETAILS, FORMULAE AND GRAPHICS



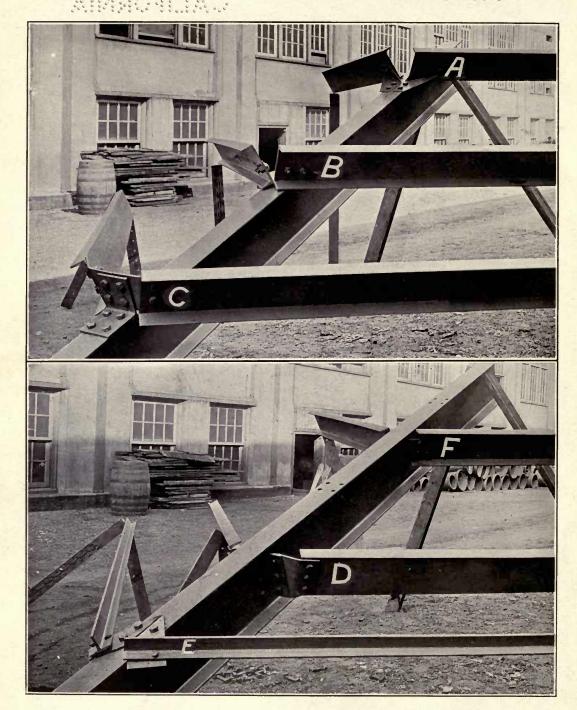








SIX STYLES OF HIP RAFTER CONNECTIONS



HIP AND VALLEY DESIGN

DETAILS, FORMULAE AND GRAPHICS

ROOFS HOPPERS AND PIPE LINES

BY

H. L. McKIBBEN and L. E. GRAY

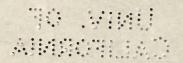
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American Bridge Company

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Second Thousand, November 1, 1913

* 201

PREFACE.

The difficulty of making working shop drawings for roof connections at Hip and Valley is appreciated by Structural Engineers.

This book has been prepared to cover practical working details for such construction and to present the analytic and graphic processes needful for their development.

From the presentation of the designs here given, Engineers and Architects can determine the style of connection adapted to their demands readily and can specify the same for the structures they have in charge.

To Draftsmen the treatment of the subject will especially appeal, resulting to them in a saving of extra labor and concern.

Students will discover the practical training in descriptive geometry and trigonometry as applied to active engineering to be exceptionally valuable. Class room work in the proof of the formulae is recommended to Engineering Schools.

H. L. McKibben.

L. E. GRAY.

Engineers with American Bridge Co.

1

FOREWORD.

On pages 3, 4 and 5 are shown working details for styles A, B, C, D, E and F, or six methods of connection to Hip Rafters from which to select the one that conforms best to the adjoining framing.

On pages 6, 7 and 8 are found working details for styles A, B, C, D, E and F, or six methods of similar connections to Valley Rafters from which to choose the one most desirable.

A sketch appears with each style of detail showing the position of the purlin in the main roof section, and small sub-formulae showing solutions for the variables y1 to y10, with special attention to y1 and y2.

After making selection of style desired, the detailer should solve the angles required as shown in details; i. e., L8 and L9 are needed in style C. No other angles need be found; only those involved in the style chosen.

Solution of these angles can be readily made from general formulae on page 10, if the worker be familiar with Trigonometry and Logarithms; if not, results may be obtained from the simple graphics given on pages 11, 12 and 13, making the problem easy for the detailer who is not familiar with formulae.

If the case in hand be one that is covered by the tabulated solutions on pages 14, 15 and 16, the worker can take from those tables any or all variables which develop in a roof of pitch ¹/₅, ¹/₄, ¹/₃, 30° or 55°, if the angle B in plan is 30°, 45° or 50°.

These tabulated solutions give the values of the variables for designs in most common use without the necessity of solving any angles whatever; but the formulae on page 10 and graphics on pages 11, 12 and 13 furnish data for solving angles for any roof pitch and all possible positions of rafter.

In styles A, B, C and E the roof line being above the main truss metal line, the worker will need to use formulae on page 9 to locate working point "d."

The authors desire to call especial attention to the following:

1st. The known data are in all cases the main roof pitch or Angle A. The position of Hip or Valley Rafter, Angle B, which is the angle formed by rafter and main truss as seen in *Plan* looking directly perpendicular to lower side of Angle A. No other data than A and B as above described is ever required.

Throughout both details and graphics the letter "d" refers always to the same working point; the marks d1 and d2 refer also to this same point, viewed from different positions.

2d. All formulae on page 10 are logarithmic, and in terms of tangent functions.

3d. Use of the graphics on pages 11,12 and 13 expedite the work and give accurate results.

4th. A short method of graphics for solution of Angles 45, 46 and 48 also appears on page 10, which may be used after solving 43 and 44, if desired.

5th. For those desiring to follow out the proofs given on pages 21 to 29, the four major intersecting planes involved are as follows (see page 10):

ROOF PLANE.

Seen in Elevation of Truss as line ab. Seen in Plan as inclined surface a1, b1, r1.

PURLIN WEB PLANE.

Seen in Elevation of Truss as line c, d. Seen in Plan as inclined surface d1, c1, e1.

RAFTER WEB PLANE.

Seen in Elevation of Rafter as surface r2, c2, b2. Seen in Plan as line r1, b1.

RAFTER FLANGE PLANE.

Seen in Elevation of Rafter as line r2, b2. Seen in Plan as inclined surface r1, b1, e1.

6th. Other formulae which may be used if desired are as follows:

Cos *L3*=Cos R Cos *L1* Sec A. Tan *L5*=Cos A Tan B Cos *L1*. Tan *L5*=Tan *L2* Cos *L1*. Tan *L7*=Sin A Sin B Cos *L4*. Tan *L7*=Cos *L2* Tan *L10*.

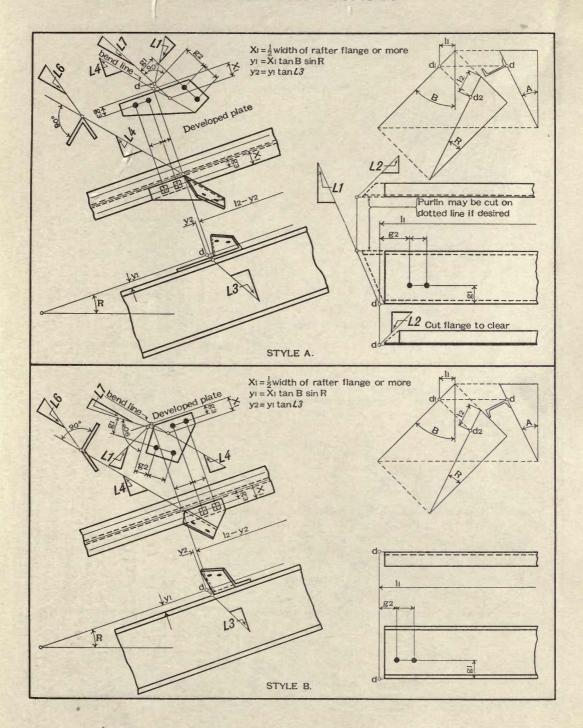
HOPPERS, BINS AND CHUTES (FORMS OF VALLEY CONSTRUCTION).

Details for these structures are left to the judgment of the detailer and are usually governed by the main design. The solution of the bend on connecting plate at dihedral intersections is the only difficulty for most draftsmen. Both formulae and graphics are provided on page 17 for ready use.

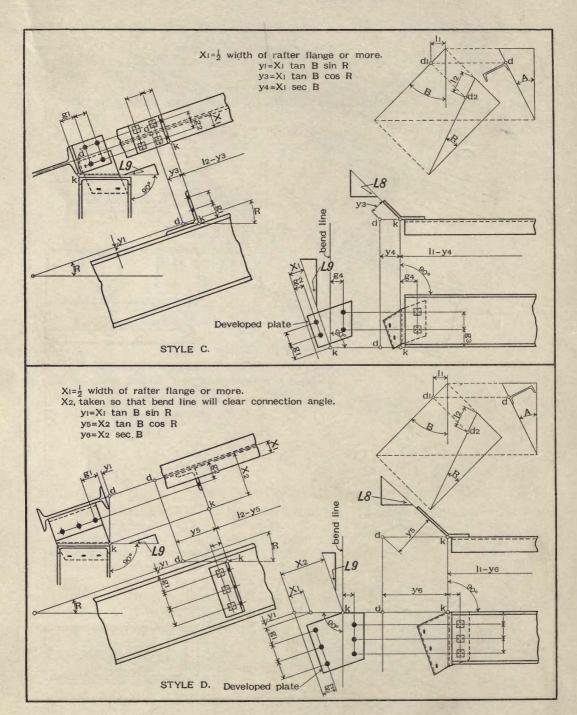
PIPE LINES.

Large Pipe Lines often require both horizontal and vertical change of direction at the same point, which condition may give rise to annoying details. Two separate bends are more expensive and produce greater friction on the flow than a single resultant bend. Careful attention to resultant angles "X" and detail angles "Y" will save much trouble in fabrication and improve the efficiency of the finished structure.

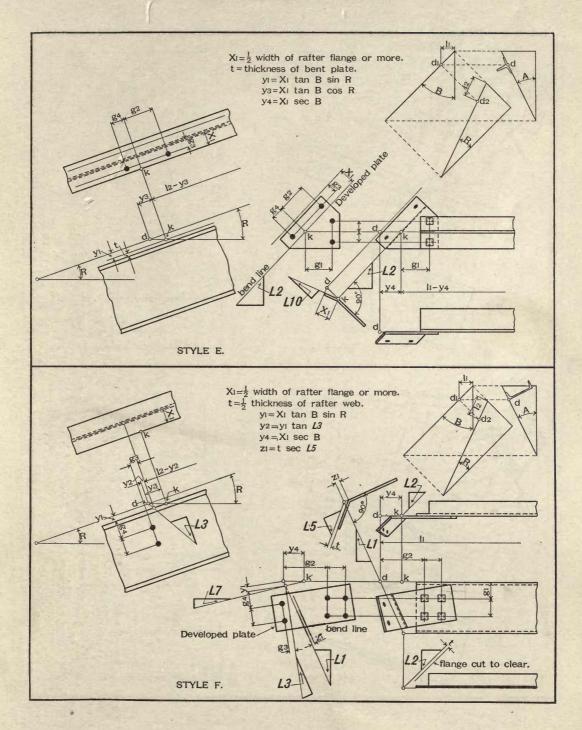
HIP RAFTER DETAILS



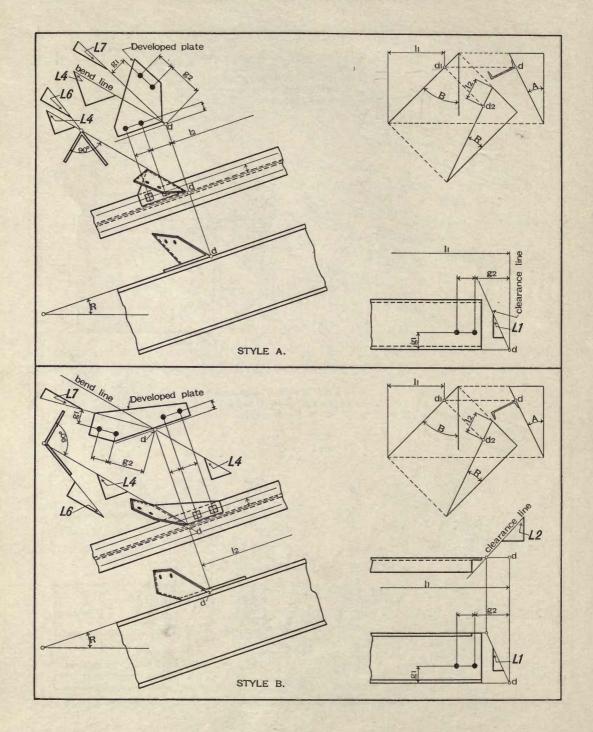
HIP RAFTER DETAILS



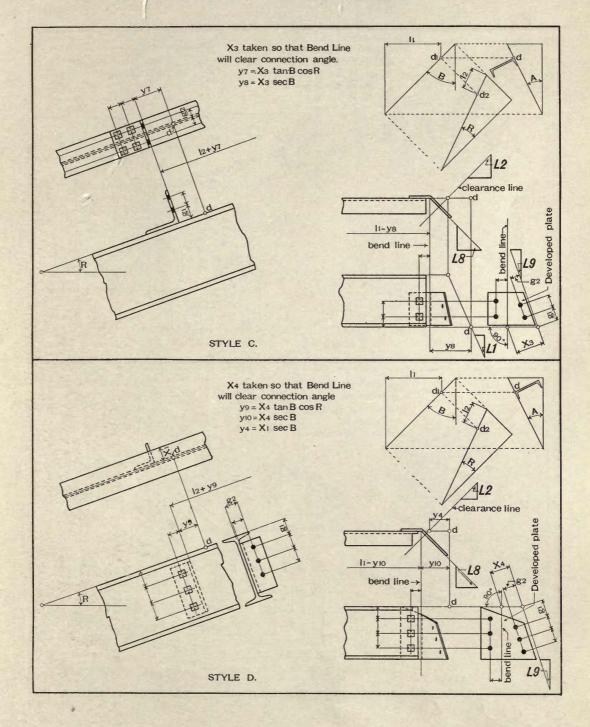
HIP RAFTER DETAILS



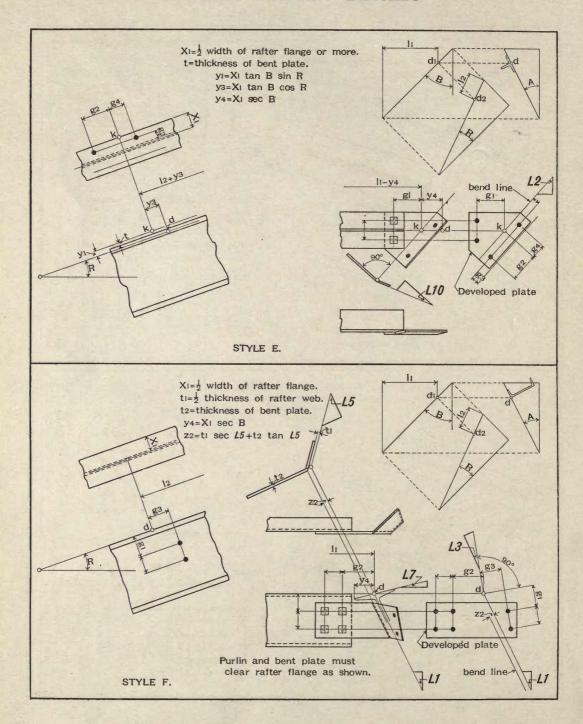
VALLEY RAFTER DETAILS



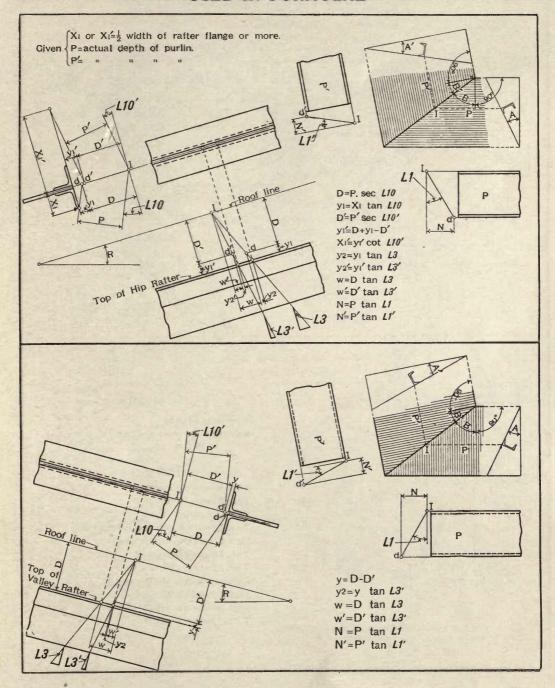
VALLEY RAFTER DETAILS



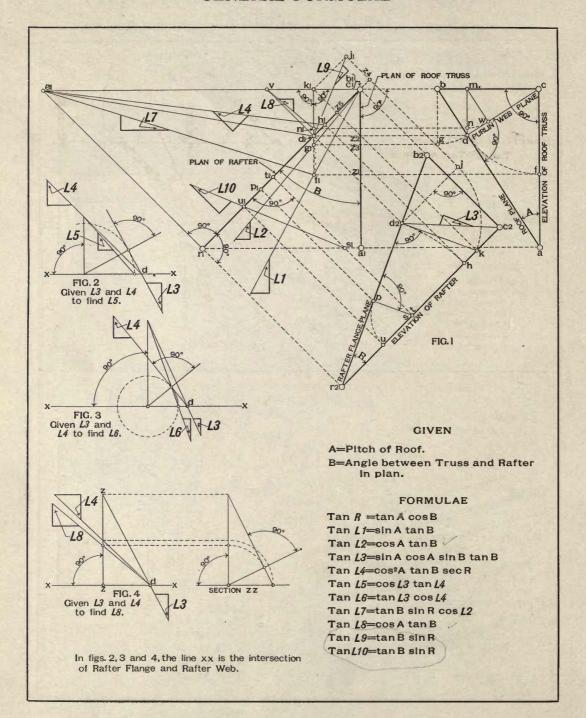
VALLEY RAFTER DETAILS



RELATIONS OF ROOF LINE TO WORKING POINTS USED IN FORMULAE



GENERAL FORMULAE



A = PITCH OF ROOF

B = ANGLE BETWEEN TRUSS AND RAFTER IN PLAN

R=PITCH OF RAFTER

Tan R=Tan A Cos B

L1—BEVEL ON PURLIN WEB PLANE MADE BY INTERSECTION OF RAFTER WEB PLANE

FORMULA
Tan L1-Sin A Tan B

GRAPHICS

Draw d, c 1 a, b

Draw d, d | b, b |

Revolve d to f, about c

Draw f, f | d, d |

Draw d |, f 1 d, d |

Connect f with c |

L2—BEVEL ON ROOF PLANE MADE BY INTERSECTION OF RAFTER WEB PLANE

FORMULA
Tan L2 - Tan B Cos A

GRAPHICS

Revolve b to g about a

Draw g, g| | b, b|

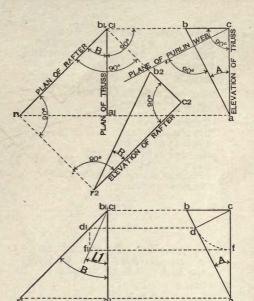
Extend a|, b| to g|

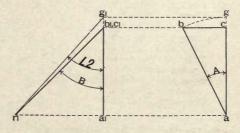
Connect g| with r|

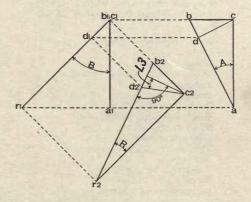
L3—BEVEL ON RAFTER WEB PLANE MADE BY INTERSECTION OF PURLIN WEB PLANE

FORMULA
Tan L3 - Sin A Cos A Sin B Tan B

GRAPHICS
Draw d, c 1 a, b
Draw d, d| | b, b|
Draw d, d2 | b|, b2
Connect d2 with c2







GRAPHIC SOLUTION OF ANGLES

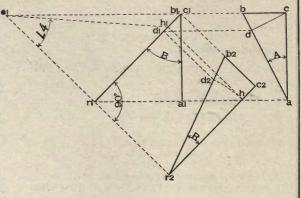
L4—BEVEL ON RAFTER FLANGE
PLANE MADE BY INTERSECTION OF PURLIN WEB
PLANE

FORMULA

TanL4 = Cos2 A Tan B Sec R

GRAPHICS

Draw d, cla, b
Draw d, dl || b, bl
Draw dl, d2 || bl, b2
Revolve d2 to h, about r2
Draw h, hl || bl, b2
Extend b, bl to intersect rl, r2 at el
Connect'el with hl



L5—COMPLEMENT OF ANGLE BETWEEN PURLIN WEB PLANE AND RAFTER WEB PLANE

FORMULA

Tan L5 = Cos L3 Tan L4

GRAPHICS

Draw d, c \perp a, b Draw d, d| \parallel b, b| Draw d| d2 \parallel b|, b2 Draw d2, z2 \perp b2, c2 Draw z2, z3 \perp d2, c2 Revolve z3 to z4 about z2 Draw z4, z5 \parallel b|, b2 Locate z6 at intersection of d, d| and c|, c2 Connect z5 with z6

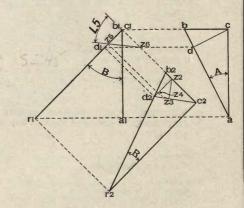
L6—COMPLEMENT OF ANGLE BE-TWEEN PURLIN WEB PLANE AND RAFTER FLANGE PLANE

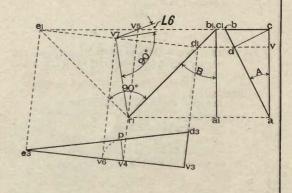
FORMULA

Tan L6 = Tan L3 Cos L4

GRAPHICS

Draw d, cla, b
Draw d, d| b, b| and extend to v
Extend b, b| to e|
Connect e| with d|
Draw e3, v3 | e|, d|
Draw e1, e3 and d|, v3 le|, d|
Take v3, d3 = d, v
Connect e3 with d3
Through r|, draw v4, v5 le|, d|
Draw v4, ple3, d3
Revolve p to v6 about v4
Draw v6, v7 le|, d|
Connect v7 with r| and v5





L7—BEVEL ON PURLIN WEB PLANE MADE BY RAFTER FLANGE PLANE

FORMULA

Tan L7 Tan B Sin R Cos L2

GRAPHICS

Draw d, c 1 a, b
Draw d, d | | b, b |
Revolve d to f about c
Draw f, f | | b, b |
Draw d | f | 1 d, d |
Extend b, b | to e |
Connect e | with f

L8—ANGLE BETWEEN PURLIN WEB PLANE AND A PLANE PERPENDICULAR TO BOTH RAFTER WEB PLANE AND RAFTER FLANGE PLANE

FORMULA

Tan L8 = Tan B, Cos A

GRAPHICS

Draw d, c l a, b Draw d, dl \parallel b, bl Draw d, m l b, c Draw m, s l d, c Revolve s to n about m Draw dl, p \parallel d, dl Draw dl, v l rl, bl to intersect b, bl at v Connect v with p

L9—BEVEL ON PLANE PERPENDICULAR TO BOTH RAFTER WEB PLANE AND RAFTER FLANGE PLANE MADE BY INTERSECTION OF PURLIN WEB PLANE

FORMULA

Tan L9 = Tan B Sin R

GRAPHICS

Draw d, c 1 a, b
Draw d, d | | b, b |
Draw d, d | | b, b |
Draw d | d | b | b, b |
Draw d | d | b | b |
Draw d | k | 1 r | b |
Revolve k to j about, d |
Draw k | j | | k, k |
Draw k | j | 1 k, k |
Connect d | with j |

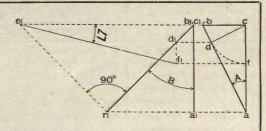
L10—ANGLE BETWEEN ROOF PLANE AND RAFTER FLANGE PLANE

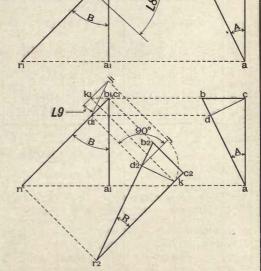
FORMULA

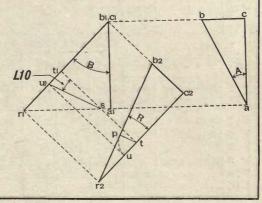
Tan L10 = Tan B Sin R

GRAPHICS

Take p any point on b2, r2
Draw p, t 1 b2, r2
Revolve p to u about t
Draw t, ti || bi, b2
Draw u, ui || bi, b2
Locate s at intersection of t, ti and a, ri
Connect ui with s







SOLUTIONS, FIVE ORDINARY ROOF PITCHES B=30°

		GIE!											4500	-			_					25%		
A	1/	5 PIT	CH	18-1		1/4	PIT	СН		30° PITCH					1/3 PITCH					55° PITCH				
><	"S"	Log	. Ta	n.	"S"	•	Log.	Tai	ı.	"S	•	Log.	Ta	n.	"S'		Log	. Ta	ın.	"S"	•	Log.	Tar	1.
R	45/82	9.5	3959	,	5%	5%18 9.63650			6	9.69897			615/1	9.76144			1427/8	32	0.0	9230				
L 1	2%16	9.3	3127	7	3%	33/32		9.41195		315/82 9.46		6041		327/82		9.50550		0	511/10	В	9.6	7480		
L 2	67/18	7.00	72921					1298		6			9897		53/4		9.68159		9	381/82		9.52003		
L 3	1%18		9801		113/8		100	6247		11/2			9691		119/8	7		1246		15%			3237	
L 4 L 5	65/18		2159		61/8			0185		5184	6		8496	7000	517/8			642		35%			8016	
L 5 L 6	6%2		71945 94484		6			9897 1344		584			8159 5119		51/2		-34	603	Carlo	31%		- 2	7620	
L 7	2		2157		27/10			0929	-	225/8	-	1000	6350		31/8)826 153		1% ₁₆			1340 2961	
L 8	67/18		72921	100	634			1298	0.00	6	2		9897	100	584	1		3815		331/8			2003	
L 9	2%2	9.2	7642	2	284		9.3	6062		3%	2		1195		315/8			604		5%			5221	
L 10	2%2	9.2	27642	2	28/4		9.3	6062		3%	2	9.4	1198	5	315/8	2		1604		5%		9.6	5221	
"8"	' = Co	rresp	ond	ing :	Beve	lso	r Slo	pes	to	Base	of	12 in	che	s.		-		-						
			DE.							1						2			-	1	-			
A	1/	5 PIT	CH			1/4	PII	CH			30	PIT	CH			1/3	PIT	CE		- 4	55°	PIT	CH	
X 1	11/2 23	2 3	41/4	61/4	1 1/2	21/2	3	41/4	61/4	1 1/2	21/2	3	41/4	61/4	11/2	2½	3	41/4	61/4	11/2	21/2	3	11/4 6	31/4
Y 1	9 1	5 9 16	18	1 8	$\frac{11}{32}$	9 18	11 16	3 1 3 2	1 7 1 6	3/8	21	25	1 3 2	15/8	7.	28	7/8	137	118	11 16	11/8	1 1 1 2	129 2	213
Y 2	1 1 1 32 1	1	3 2	1/8	1 32	16	1 6 8 3 2	1/8	5 32	1 16	3 2 3 2		1/8	3 16	1	3 2 3 2	1/8	5 3 2	1/4	16 3 32	5 32	3 16		3/8
Y 3	18 13			318		1 5 6			3 5		1 9 2		2 3 1 6		3/4		11/2				29		1 1 7 2	
Y 4	133 27		$4\frac{29}{32}$	$7\frac{7}{32}$		27/8		429		123	27/8		429						7 7 3 2				432	
A	For Purlins not exceeding 12" Depth, with 4½" Connection Clearance, the following assigned values of X ₂ , X ₃ , X ₄ , give good Results. Y ₅ to Y ₁₀ derived therefrom. CLEARANCES FOR 9 INCH PURLIN A 1/5 PITCH 1/4 PITCH 30° PITCH 1/3 PITCH 55° PITCH																							
-	-/		1			-/-	111	UH		2	30	FI	LOB			1/3	PII	CH			00	PIT	CH	_
X	X2=	X3=	1	4=	X2=		X3=	X4		X2=	-	X3=	X4		X2=		K 3=		4=	$X_2 =$	2	Z 3=	X4	
	6½	5	4	1/2	63/4		5	4	1/2	7		5	4	1/2	71/4		5	4	1/2	81/2		5	41	2
Y 5	317/82				3%	3				35/8					35/8					33/82				
Y 6	71/2				725%					88/82					83%					91%16				
Y 7		228/82		• • • • •			221/82					21%2					21/2				1	13/16		
Y 8		525/82		e/			525/82			• • • • • •		525/32			• • • • • •	8	25/82			• • • • • •	5	25/82		
Y10			- 33	5/32 3/16				. 2	%8 148	• • • • • •	••••	• • • • • •	. 25			••••	• • • • •		21/4	• • • • • •		• • • • •	15	
110			. 0	716	CIT		RA			FC		10	-	18	DI		TAT	-	3/16		• • • •	• • • • • •	5%	.6
	1/1							-	E O					UH	PU				1	0				
A	1/:	5 PIT	CH			1/4	PIT	CH	10	3	10°	PIT	CH			1/3	PIT	CH		- 6	55°	PIT	CH	
X	X2=	X3=		4=	X2=		$X_3 =$	X4		X2=		X3=	X	- 1	X2=		Z3=		4=	X2=		Z3=	X4:	_
	7	7½	4	1/2	71/2	-	71/2	4	/2	8		71/2	4	1/2	81/2		$7\frac{1}{2}$	4	1/2	10		7½	41/	2
Y 5	31%16				381/8					41/8					41/4					35%				
Y 6	8%2				821/3					91/4					91%					11%16				
Y 7	• • • • • • • •	48/82					381/82					37/8					3%					28/32		
Y 8	• • • • • • • •	821/82		×/		1	B ² 1/8 ₂				8	821/82			• • • • • •	8	21/82				. 8	21/82		•••
Y10				%2 %82	• • • • • •	•		53		• • • • • •				18	• • • • • •	•	• • • • •	1	1/4	•••••			15%	_
- 10			. 0	718				09	16				. Da	48				. 0	%ie .				5%	16

SOLUTIONS, FIVE ORDINARY ROOF PITCHES

A	1/5	PITCH	1/4	PITCH	30	° PITCH	1/3	3 PITCH	55° PITCH		
> <	"S" Log. Tan.		"s"	Log. Tan.	"s"	Log. Tan.	"s"	Log. Tan.	"s"	Log. Tan.	
R	313/32	9.45154	41/4	9.54845	47/8	9.61092	521/32	9.67339	121/8	0.00426	
L 1	415/32	9.56983	53%	9.65051	6	9.69897	621/82	9.74406	927/32	9.91336	
L 2	115/32	9.96777	10%	9.95154	1013/32	9.93753	10	9.92015	67/8	9.75859	
L 3	215/16	9.38709	3%	9.45154	311/16	9.48599	32%2	9.51369	4	9.52144	
L 4	10%	9.95225	10%18	9.92867	923/82	9.90853	93/16	9.88387	55/8	9.66984	
L 5	107/16	9.93971	918/16	9.91195	95/16	9.88908	823/82	9.86190	55/18	9.64710	
L 6	23/18	9.25914	21%2	9.33379	227/82	9.37641	31/8	9.41357	35/8	9.47851	
L 7	218/82	9.29984	281/32	9.39524	37/18	9.45593	315/16	9.51558	718/82	9.78984	
L 8	115/32	9.96777	10%	9.95154	1013/32	9.93753	10	9.92015	67/8	9.75859	
L 9	31/4	9.43483	4	9.52288	417/82	9.57745	51/8	9.62982	817/32	9.85160	
L 10	31/4	9.43483	4	9.52288	417/82	9.57745	51/8	9.62982	817/82	9.85160	
" 5	3" - C	orresponding	Bevels	or Slopes to	Base of	12 inches.	-0-01		enne-		
A	1/5	PITCH	1/4	PITCH	30	° PITCH	1/3	PITCH	55	° PITCH	

	1		1/5	PIT	CH			1/4	PIT	сн			30°	PI	CE		1	/3 :	PIT	сн			55°	PI	гсн	
x	1	1 ½	21/2	3	41/4	61/4	1 1/2	2½	3	41/4	61/4	11/2	21/2	3	41/4	61/4	11/2	2½	3	41/4	61/4	1½	2½	3	41/4	61/4
Y	1 2	$\frac{13}{32}$	11 16 5 32	13 16 3 16	1 5/3 2 9/3 2	1 1 1 6 1 3 3 3	-	0.0	1 9 3 2	$1\frac{1}{3}\frac{3}{2}$ $\frac{1}{3}\frac{3}{2}$	2 3 2 1 9 3 2		15 16 9 32	1½ 1½ 11/32			5/8 7 3 2	$1\frac{1}{16}$ $\frac{1}{3}\frac{1}{2}$				$1\frac{1}{16}$ $\frac{1}{32}$	$1\frac{25}{32}$ $\frac{19}{32}$	2½ 2½ 23 32	3 1 1 1	4 ₁₆ 1 ¹⁵ / ₃
Y	3 4		$2\frac{1}{3}\frac{3}{2}$	2 1/8		6	$1\frac{1}{3}\frac{3}{2}$	$2\frac{1}{3}\frac{1}{2}$	$2\frac{27}{32}$	4	5 2 9 2	13/8	216	$2\frac{25}{32}$	315	$5\frac{25}{32}$	$1\frac{1}{3}\frac{1}{2}$ $2\frac{1}{8}$	21/4	$2\frac{2}{3}\frac{3}{2}$	$3\frac{27}{32}$		1 1 6	13/4			$4\frac{1}{3}\frac{3}{2} \\ 8\frac{2}{3}\frac{7}{2}$

For Purlins not exceeding 12" Depth, with $4\frac{1}{2}$ " Connection Clearance, the following assigned values of X_2 , X_3 , X_4 give good Results. Y_5 to Y_{10} derived therefrom.

CLEARANCES FOR 9 INCH PURLIN

A	1/5 PITCH 1/4 PITCH				н	30	° PITC	OH.	1/	3 PITC	н	55° PITCH			
X	X ₂ = 7	X ₃ = 5½	X ₄ = 4½		X ₃ = 5½	X ₄ = 4½		X ₃ = 5½	X ₄ = 4½	X ₂ = 8½	X ₃ = 5½	X ₄ = 4½	X ₂ =	X ₃ = 5½	X ₄ = 4½
Y 5															
Y 7		5%2			53/16			58/82		• • • • • • • • • • • • • • • • • • • •	481/82			37/8	
Y 9	100 000		411/82			41/4			45/82				• • • • • • • • • • • • • • • • • • • •		35/82

CLEARANCES FOR 12 INCH PURLIN

A	1	1/5 PITCH			1/4 PITCH			30	30° PITCH			3 PIT	CH	55° PITCH		
X		X ₂ =	X ₃ = 7½	X ₄ = 4½		X ₃ = 7½		x ₂ =		X ₄ = 4½			$X_4 = 4\frac{1}{2}$	$X_2 = 11\frac{1}{2}$		X ₄ = 4½
YE	- 1													200000000000000000000000000000000000000		
1000			77/32			71/18			615/18			625/82				
Y	9			411/82			41/4		-	45/82						35/82

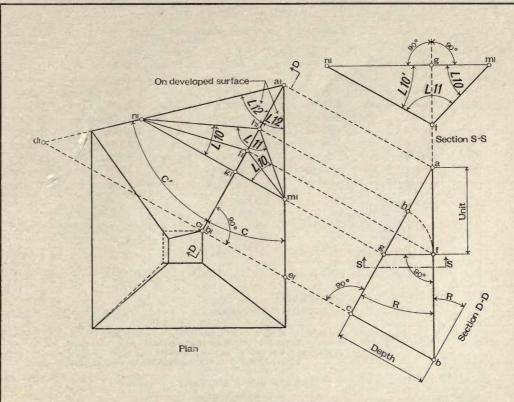
SOLUTIONS, FIVE ORDINARY ROOF PITCHES

B=50°

A	1/	1/5 PITCH 1/4 PITCE				0° PITCH	1/	3 PITCH	5	55° PITCH		
><	"S"	Log. Tan.	"S"	Log. Tan	. "S"	Log. Tan.	"S"	Log. Tan.	"S"	Log. Tan.		
R	33/82	9.41013	327/82	9.50704	415/32	9.56951	55/32	9.63198	11	9.96284		
L 1	55/16	9.64602	613/32	9.72670	75/82	9.77516	715/16	9.82024	1123/32	9.98955		
L 2	13%2	0.04396	1225/82	0.02773	12%	0.01372	1129/82	9.99634	8%16	9.83478		
L 3	325/32	9.49804	43%	9.56250	48/4	9.59694	51/16	9.62465	55/82	9.63240		
L 4	1223/32	0.02563	121/82	0.00062	117/16	9.97927	1025/82	9.95309	63/8	9.72610		
L 5	12%2	0.00511	11%2	9.97344	105/8	9.94775	915/18	9.91761	57/8	9.68942		
L 6	219/82	9.33433	38/82	9.41167	37/16	9.45655	3%	9.49632	417/32	9.57824		
L 7	23/8	9.29881	3	9.39706	315/32	9.46025	4	9.52286	8	9.82305		
L 8	13%2	0.04396	1225/32	0.02773	12%	0.01372	1129/32	9.99634	8%16	9.83478		
L 9	3%16	9.47241	4%	9.56188	481/82	9.61767	55/8	9.67155	921/82	9.90630		
L 10	3%18	9.47241	43%	9.56188	481/82	9.61767	5%	9.67155	921/82	9.90630		
"S	"=Cor	responding	Bevels	or Slopes	to Base o	of 12 inches.						
A	1/	5 PITCH	1,	4 PITCH	30	O° PITCH	1/	3 PITCH	58	° PITCH		
X 1	11/2 2	3 41/4 61/	4 11/2 2	1/2 3 41/4 6	1/2 2	1/2 3 41/4 61/4	11/221	2 3 41/4 61/4	11/22	3 41/4 61/4		
Y 1	7 3	4 29 11/4 12	7 9 2	9 13 19 2	9 5/8 1	1 11/4 13/4 21/9 3 2 11/4 13/4 21/9	23 1 ₁	$\frac{3}{6}$ $1\frac{13}{32}$ 2 $2\frac{15}{6}$	1 3 2	2 2 3 3 3 7 5 1 2		
Y 2	5 1	4 0 40 0				$\frac{8}{2}$ $\frac{1}{2}$ $\frac{11}{16}$ $1\frac{1}{32}$				$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		
Y 3	0 - 1	$783\frac{15}{32}4\frac{29}{32}7_3$				$\frac{25}{32}$ $3\frac{11}{32}$ $4\frac{3}{4}$ $6\frac{31}{32}$				8 25/8 323 51/2		
Y 4		1/8 4 ² 1/ ₃ 2 65/8 9 ² 3	$\frac{3}{2}$ $2\frac{11}{32}$ 3	7/8 421 65/8 S	$\frac{23}{32}$ $2\frac{1}{32}$ 3	7/8 421 65/8 923 2 65/8 923	211 37	8 421 65/8 933	$2\frac{1}{3}\frac{1}{2}$ 3	8 421 65/8 923 2 65/8 932		
A	For Purlins not exceeding 12" Depth, with $4\frac{1}{7}$ " Connection Clearance, the following assigned values of X_2 , X_3 , X_4 , give good results. Y_5 to Y_{10} derived therefrom. CLEARANCES FOR 9 INCH PURLIN A 1/5 PITCH 1/4 PITCH 30° PITCH 1/3 PITCH 55° PITCH											
1		2 LITOH		4 PITUH	- 0	O PITCH		3 FIIOH	5	5° PITCH		
1	-	1		1			-		-			
X	X2=	X3= X4=	X2=	X3= X4	= X ₂ =	X3= X4=	X2=	X3= X4=	X2=	X3= X4=		
X	X ₂ = 7½	1		1	= X ₂ =		-		-			
Y 5		X3= X4=	X ₂ =	X3= X4	$x_{2} = x_{2} = 8\frac{1}{2}$	X3= X4=	X2=	X3= X4=	X ₂ = 10½	X3= X4=		
Y 5 Y 6	71/2	$X_3 = X_4 = 5\frac{1}{2}$ $4\frac{1}{2}$	X ₂ = 8 9½16	$X_3 = X_4$ $5\frac{1}{2}$ $4\frac{1}{2}$	$x_2 = x_2 $	X ₃ = X ₄ = 5½ 4½	X ₂ = 9 9 ²⁷ / ₈₂	$X_3 = X_4 = 5\frac{1}{2}$ $4\frac{1}{2}$	$X_2 = 10\frac{1}{2}$	$X_3 = X_4 = 5\frac{1}{2}$ $4\frac{1}{2}$		
10000	7½ 821/82	X ₃ = X ₄ = 5½ 4½	X ₂ = 8 9½6	X ₃ = X ₄ 5½ 4½ 6¼	$x_2 = x_2 = 8\frac{1}{2}$ $x_2 = 8\frac{1}{2}$ $x_2 = 8\frac{1}{2}$	X ₃ = X ₄ = 5½ 4½	X ₂ = 9 9 ²⁷ / ₈₂	X ₈ = X ₄ = 5½ 4½	$X_2 = 10\frac{1}{2}$	X ₃ = X ₄ = 5½ 4½		
Y 6 Y 7 Y 8	7½ 821/32 1121/32	X ₃ = X ₄ = 5½ 4½ 61½ 8%6	X ₂ = 8 9½6 12½6	X ₃ = X ₄ 5½ 4½ 6¼ 8%6	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	X ₃ = X ₄ = 5½ 4½ 6% ₂	X ₂ = 9 9 ²⁷ / ₈₂ 14	X ₃ = X ₄ = 5½ 4½ 6½ 2	$X_2 = 10\frac{1}{2}$ $9\frac{1}{2}$ $16\frac{1}{3}$	$X_3 = X_4 = 5\frac{1}{2}$ $4\frac{1}{2}$ $4^2\frac{1}{2}$ $8\frac{1}{2}$		
Y 6 Y 7 Y 8 Y 9	7½ 821/32 1121/32	X ₃ = X ₄ = 5½ 4½ 61½ 4½ 61½ 5¾6 5¾6	X ₂ = 8 9¼6 12¾6	X ₃ = X ₄ ; 5½ 4½ 6¼ 8%6	$x_2 = x_2 $	X ₃ = X ₄ = 5½ 4½ 6%2	X ₂ = 9 9 ²⁷ / ₈₂ 14	X ₃ = X ₄ = 5½ 4½ 6½ 8%6 41%6	X ₂ = 10½ 9% ₂ . 16½ . 16½	X ₃ = X ₄ = 5½ 4½ 4½ 4 ²⁷ / ₈₂		
Y 6 Y 7 Y 8	7½ 821/32 1121/32	X ₃ = X ₄ = 5½ 4½ 61½ 8%6	X ₂ = 8 9½s 12½s	X ₃ = X ₄ 5½ 4½ 6¼ 8%6	$x_2 = x_2 $	X ₃ = X ₄ = 5½ 4½ 6% ₂	X ₂ = 9 9 ²⁷ / ₈₂ 14	X ₃ = X ₄ = 5½ 4½ 6½ 2	$X_2 = 10\frac{1}{2}$ $9\frac{1}{2}$ $16\frac{1}{3}$	X ₃ = X ₄ = 5½ 4½ 4½ 4 ²⁷ / ₈₂		
Y 6 Y 7 Y 8 Y 9	7½ 821/32 1121/32	X ₃ = X ₄ = 5½ 4½ 61½ 4½ 61½ 5¾6 5¾6	X ₂ = 8 9½6 12¾6	X ₃ = X ₄ ; 5½ 4½ 6¼ 8%6 5%	= X ₂ = 8½ 8½ 9½ 13½ 13½	X ₃ = X ₄ = 5½ 4½ 6%2	X ₂ = 9 9 ^{27/82} 14	X ₃ = X ₄ = 5½ 4½ 6½ 8½ 4½,7	X ₂ = 10½ 9% ₂ . 16½ . 16½	X ₃ = X ₄ = 5½ 4½ 4½ 4 ²⁷ / ₈₂		
Y 6 Y 7 Y 8 Y 9	7½ 821/82 1121/82	X ₃ = X ₄ = 5½ 4½ 61½ 4½ 61½ 5¾6 5¾6	X ₂ = 8 9½6 12½6	X ₃ = X ₄ ; 5½ 4½ 6¼ 8%6 5%	= X ₂ = 8½ 9½ 13½ 13 52	X ₃ = X ₄ = 5½ 4½ 65½ 8%6 5½2	X ₂ = 9 9 ²⁷ / ₅₂ 14	X ₃ = X ₄ = 5½ 4½ 6½ 8½ 4½,7	X ₂ = 10½ 10½ 9½ 16½ 16½	X ₃ = X ₄ = 5½ 4½ 4½ 4 ²⁷ / ₈₂		
Y 6 Y 7 Y 8 Y 9 Y10	7½ 821/82 1121/82	X ₃ = X ₄ = 5½ 4½ 6½ 4½ 6½ 5½ 7	X ₂ = 8 9½6 12½6 CLE 1 X ₂ =	X ₃ = X ₄ 5½ 4½ 6¼	$X_2 = X_2 = 8\frac{1}{2}$ $8\frac{1}{2}$ $13\frac{1}{2}$ $13\frac{1}{2}$ $13\frac{1}{2}$ $13\frac{1}{2}$ $13\frac{1}{2}$ $13\frac{1}{2}$ $13\frac{1}{2}$	X ₃ = X ₄ = 5½ 4½ . 6½ 4½ . 8½	X ₂ = 9 9 ²⁷ / ₅₂ 14	X ₃ = X ₄ = 5½ 4½ 6½ 2 8%6 4½7 7	X ₂ = 10½ 10½ 9½ 16½ 16½	X ₃ = X ₄ = 5½ 4½ 4½ 4½ 4½		
Y 6 Y 7 Y 8 Y 9 Y10	7½ 82½2 112½2 112½2	X ₃ = X ₄ = 5½ 4½ 61½2 61½2 8¾6 7 /5 PITCH X ₃ = X ₄ =	X ₂ = 8 9½6 12½6	X ₃ = X ₄ 5½ 4½ 6¼ 6¼ 5% 7 EARANC: /4 PITCH X ₃ = X ₄ 7½ 4½	ES FOI	X ₃ = X ₄ = 5½ 4½	X ₂ = 9 9 ²⁷ / ₅₂ 14 1/	X ₃ = X ₄ = 5½ 4½ 6½ 4½ 8½ 7 RLIN X ₃ = X ₄ = 4½ X ₄ = 4½	X ₂ = 10½ 9% 16½ 16½ 16½ X ₂ = 12½	X ₃ = X ₄ = 5½ 4½ 4 ²⁷ / ₈₂		
Y 6 Y 7 Y 8 Y 9 Y10	7½ 82½2 112½2 112½2 1	X ₃ = X ₄ = 5½ 4½ 6½ 4½ 6½ 5¾ 6¼ 7 7 7 7 75 PITCH X ₃ = X ₄ = 7½ 4½ 4½	X ₂ = 8 9½6 12½6 12½6	X ₃ = X ₄ 5½ 4½ 6¼ 6¼ 5% 7 EARANC: /4 PITCH X ₃ = X ₄ 7½ 4½	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	X ₃ = X ₄ = 5½ 4½ . 6½ 4½ . 6½	X ₂ = 9 9 ²⁷ / ₅₂ 14 14 1/	X ₃ = X ₄ = 5½ 4½ 6½ 4½ 8½ 7 RLIN X ₃ = X ₄ = 4½ 7 RLIN	X ₂ = 10½ 9%2 16½ 16½ 16½ 50 X ₂ = 12½ 108⅓2	X ₃ = X ₄ = 5½ 4½ 4 ²⁷ / ₈₂		
Y 6 Y 7 Y 8 Y 9 Y10	7½ 82½2 112½2 112½2 112½2 112½2 112½2 112½2 112½2	X ₃ = X ₄ = 5½ 4½ 6½ 4½ 6½ 5¾ 6¼ 7 7 7 75 PITCH X ₃ = X ₄ = 7½ 4½ 4½	X ₂ = 8 9½6 12½6 12½6	X ₃ = X ₄ 5½ 4½ 6¼ 8%6 7 BARANC /4 PITCH X ₃ = X ₄ 7½ 4½	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	X ₃ = X ₄ = 5½ 4½ 6½ 4½ . 6½	X ₂ = 9 9 ²⁷ / ₅₂ 14 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	X ₃ = X ₄ = 5½ 4½ 6½ 4½ 8½ 7 RLIN X ₃ = X ₄ = 4½ 7 RLIN X ₃ = X ₄ = 7½ 4½	X ₂ = 10 ¹ / ₂ 9% ₂ 16 ¹ / ₈ 16 ¹ / ₈ X ₂ = 12 ¹ / ₂ 10 ⁸ / ₈ 19 ⁷ / ₁₆	X ₃ = X ₄ = 5½ 4½ 5½ 4½ 42½ 8%		
Y 6 Y 7 Y 8 Y 9 Y10	7½ 82½2 112½2 112½2 112½2 112½2 112½2 112½2	X ₃ = X ₄ = 5½ 4½ 6½ 4½ 6½ 5¾ 6¼ 7 7 7 75 PITCH X ₃ = X ₄ = 7½ 4½ 8½ 8½ 8½ 8½ 8½ 8½ 8½ 8½ 8	X ₂ = 8 9½6 12½6 12½6 1	X ₃ = X ₄ 5½ 4½ 	ES FOI	X ₃ = X ₄ = 5½ 4½ . 6% ₂	X ₂ = 9 9 ^{27/62} 14 H PUH 1/ X ₂ = 10 10 ^{81/62} 15 ⁹ / ₁₆	X ₃ = X ₄ = 5½ 4½ 6½ 4½ 8½ 5½ 7 RLIN X ₃ = X ₄ = 7½ 4½ 8½ 4½	X ₂ = 10½ 9%2 16½ 16½ 16½ X ₂ = 12½ 108½ 19½ 19½	X ₃ = X ₄ = 5½ 4½ 5½ 4½ 42½ 8½		
Y 6 Y 7 Y 8 Y 9 Y 10 A Y 5 Y 6 Y 7 Y 8	7½ 82½2 112½2 112½2 112½2 112½2 112½2 112½2	X ₃ = X ₄ = 5½ 4½ 4½ 4½ 4½ 4½ 5½ 61½ 61½ 61½ 61½ 61½ 61½ 61½ 61½ 61½ 61	X ₂ = 8 9½6 12½6 12½6	X ₃ = X ₄ 5½ 4½ 6¼ 6¼ 5% 7 BARANC /4 PITCH X ₃ = X ₄ 7½ 4½ 8½ 11 ² ½ ₂	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	X ₃ = X ₄ = 5½ 4½ . 6% ₂	X ₂ = 9 9 ²⁷ / ₃ 2 14 H PUH 1/ X ₂ = 10 10 ⁸ / ₉ 2 15 ⁹ / ₁₆	X ₃ = X ₄ = 5½ 4½ 6½ 4½ 8½ 8½ 7 RLIN X ₃ = X ₄ = 7½ 4½ 8½ 4½	X ₂ = 10½ 9% 16½ 16½ 16½ 16½ 16½ 10½ 10½ 10½ 10½ 10½ 10½ 10½ 10½ 10½ 10	X ₃ = X ₄ = 5½ 4½ 5½ 4½ 42½ 8½		
Y 6 Y 7 Y 8 Y 9 Y10	7½ 82½2 112½2 112½2 112½2 112½2 112½2	X ₃ = X ₄ = 5½ 4½ 5½ 4½ 61½ ₃₂ 8% 6 5¾ 7 7 7 7 7 7 7 7 7 82½ ₂ 112½ ₂	X ₂ = 8 9½6 12½6 12½6	X ₃ = X ₄ 5½ 4½ . 6¼	ES FOI	X ₃ = X ₄ = 5½ 4½ . 6% ₂	X ₂ = 9 9 ^{27/62} 14 H PUH 1/ X ₂ = 10 10 ^{81/62} 15 ⁹ / ₁₆	X ₃ = X ₄ = 5½ 4½ 6½ 4½ 8½ 5½ 4½ 8½ 415/16 7 RLIN X ₃ = X ₄ = 7½ 4½ 8½ 4½ 11½ 42 415/16	X ₂ = 10½ 9% 16½ 16½ 16½ 16½ 16½ 10½ 10½ 10½ 10½ 10½ 10½ 10½ 10½ 10½ 10	X ₃ = X ₄ = 5½ 4½ 5½ 4½ 42½ 8%6		

HOPPERS, BINS AND CHUTES

FORMULAE AND GRAPHICS FOR SOLUTION OF ANGLES



EXPLANATION

Inclined surfaces al, bl, el, and al, bl, dl, intersect on line al, bl, forming dihedral angle measured by angle L11. (See Section S-S.)

Vertical section a, b, c, (Section D-D) divides the dihedral into two dihedrals, of which L10 and L10 are respectively the complements.

Angles R, C and C' must be determined from design.

Rectangular bottom with irregular top will produce slightly warped side surfaces, see dotted lines for this condition.

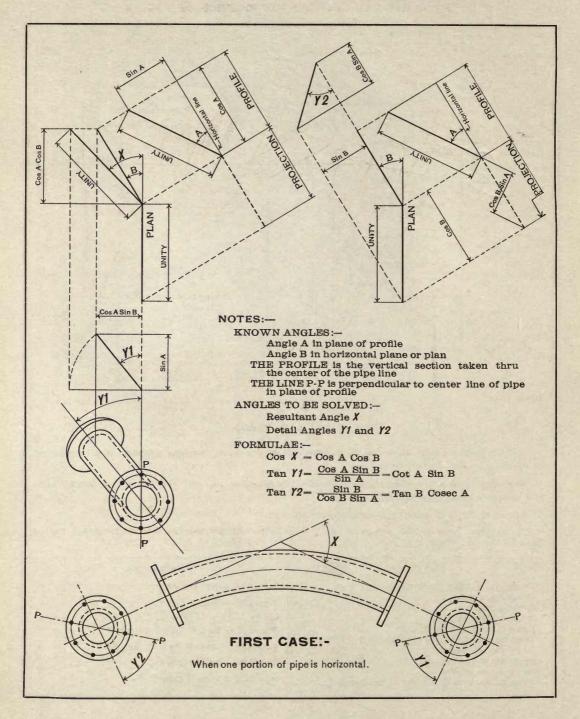
GRAPHICS

Choose any point f in line a, b
Draw f, g, 1 a, b
Draw g, n 1 a, c
Project f to f in plan
Draw fl, m | and fl, n | in plan
Then m |, n |, f | is plan of Section S-S
Revolve f to h about g
Project h to h in plan
Draw h |, m |, and h |, n |
Then h |, m |, n | is true view of Section S-S

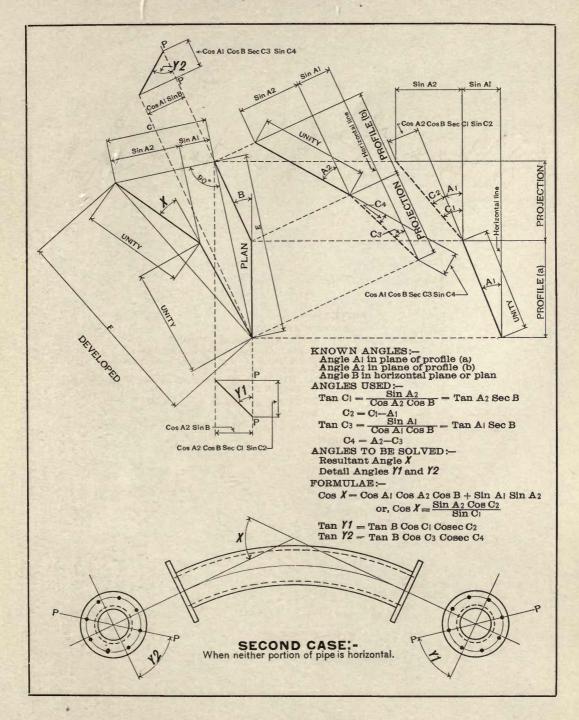
FORMULAE

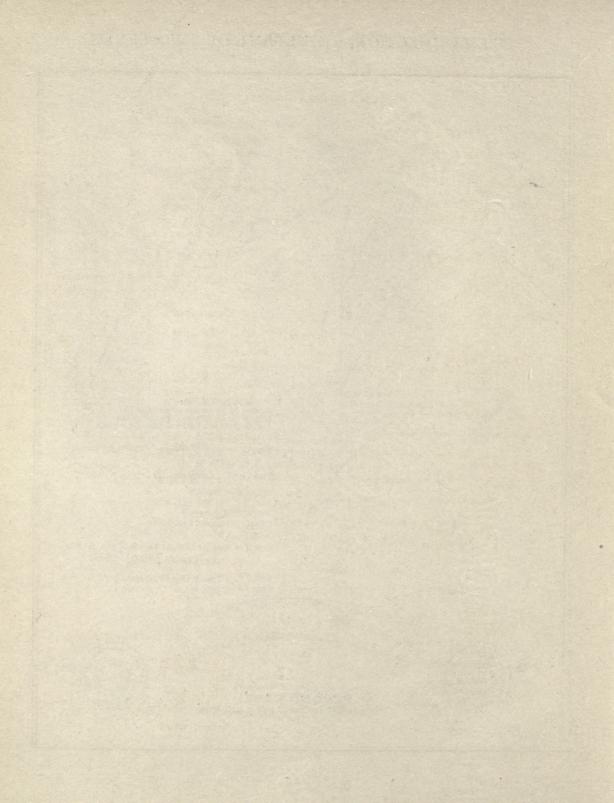
Tan L10 – Sin R Cot C Tan L10' – Sin R Cot C' L11 = 180° – (L10 + L10')Tan L12 – Sec R Tan C Sec L10Tan L12' – Sec R Tan C' Sec L10'Cos L12 = Cos R Cos C Cos L12' – Cos R Cos C'

PIPE CONNECTION, RESULTANT OF TWO BENDS



PIPE CONNECTION, RESULTANT OF TWO BENDS





Refer to Page 10; a c = unity.

Tangent R

 $\begin{array}{c} \operatorname{Tan} R = & \frac{\mathbf{c}_2, \ \mathbf{b}_2}{\mathbf{c}_2, \ \mathbf{r}_2} \\ \mathbf{c}_2, \ \mathbf{b}_2 = & \mathbf{c}, \ \mathbf{b} \\ = & \operatorname{Tan} \mathbf{A} \\ \mathbf{c}_2, \ \mathbf{r}_2 = & \mathbf{c}_1, \ \mathbf{r}_1 \\ = & \operatorname{Sec} \mathbf{B} \\ \therefore \operatorname{Tan} \mathbf{R} = & \frac{\operatorname{Tan} \mathbf{A}}{\operatorname{Sec} \mathbf{B}} \\ = & \operatorname{Tan} \mathbf{A} \operatorname{Cos} \mathbf{B} \end{array}$

Tangent L1

 $\begin{array}{c} \operatorname{Tan} L f = \frac{f!}{f_1}, \frac{Z!}{c!} \\ f!, z! = d!, z_2 \\ = (d, m) \operatorname{Tan} B \\ \operatorname{But} d, m = \operatorname{Sin}^2 A \\ \therefore f!, z! = \operatorname{Sin}^2 A \operatorname{Tan} B \\ f, c = d, c \\ = \operatorname{Sin} A \\ \therefore \operatorname{Tan} L f = \frac{\operatorname{Sin}^2 A \operatorname{Tan} B}{\operatorname{Sin} A \operatorname{Tan} B} \\ = \operatorname{Sin} A \operatorname{Tan} B \end{array}$

Tangent L2

Tan $L2 = \frac{gl, Z_3}{b, g}$ $g^l, Z_3 = dl, Z_2$ = (d, m) Tan B

But d, $m = \sin^2 A$ $\therefore gl, Z_3 = \sin^2 A$ Tan B b, g = b, d = (d, c) Tan A $= \sin A$ Tan A \therefore Tan $L2 = \frac{\sin^2 A}{\sin A}$ Tan B $= \frac{\sin A}{\tan B}$ $= \cos A$ Tan B

Tangent L4

Tan $L4 = \frac{\text{rl}, \text{ hl}}{|\text{rl}, \text{ el}}$ rl, h|=r2, h
=r2, d2
=Cos² A Sec B Sec R
rl, e|=Csc B $\therefore \text{Tan } L4 = \frac{\text{Cos}^2 \text{ A Sec B Sec R}}{\text{Csc B}}$ $= \frac{\text{Cos}^2 \text{ A Sin B}}{\text{Cos B Cos R}}$ $= \text{Cos}^2 \text{ A Tan B Sec R}$

Tangent L7

Tan $L7 = \frac{f|, k|}{e|, k|}$ fl, k|=c, f
=d, c
=Sin A
a, d=Cos A
r₂, d₂=(a, d) Sec L2
=Cos A Sec L2
r₂, k=(r₃, d₂) Sec R
el, k|=(r₃, k) Csc B
=Cos A Sec L2 Sec R Csc B
Sin A
∴Tan L7=
Cos A Sec L2 Sec R Csc B
=Tan A Cos L2 Cos R Sin B
=Tan A $\left(\frac{\sin R}{\tan R}\right)$ Tan B Cos B CosL2

Tan A Sin R Tan B Cos B CosL2

Tan A Cos B
=Sin R Tan B Cos B

Tangent L8

 $\begin{array}{c} \operatorname{Tan} \mathcal{L} \mathcal{S} = & \operatorname{nl}, \, \operatorname{kl} \\ \operatorname{nl}, \, \operatorname{kl} = \operatorname{n}, \, \operatorname{m} \\ & = \operatorname{ml}, \, \operatorname{w} \\ & = (\operatorname{d}, \, \operatorname{m}) \, \operatorname{Cos} \, \operatorname{A} \\ & = \operatorname{Sin}^2 \operatorname{A} \, \operatorname{Cos} \, \operatorname{A} \\ \operatorname{kl}, \, \operatorname{v} = (\operatorname{dl}, \, \operatorname{kl}) \, \operatorname{Cot} \, \operatorname{B} \\ & = (\operatorname{d}, \, \operatorname{m}) \, \operatorname{Cot} \, \operatorname{B} \\ & = \operatorname{Sin}^2 \operatorname{A} \, \operatorname{Cot} \, \operatorname{B} \\ & : \cdot \operatorname{Tan} \, \mathcal{L} \mathcal{S} = & \operatorname{Sin}^2 \operatorname{A} \, \operatorname{Cot} \, \operatorname{B} \\ & = \operatorname{Cos} \operatorname{A} \, \operatorname{Tan} \, \operatorname{B} \end{array}$

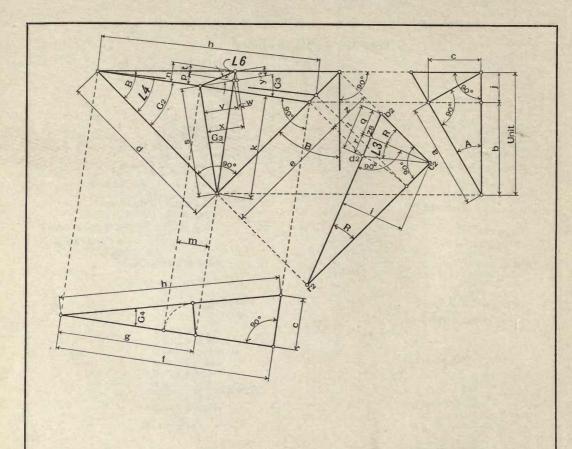
Tangent L9

Tan $L9 = \frac{\text{jl. } z_4}{\text{dl. } z_4}$ $\text{dl. } z_4 = \text{dz. } \text{j. } \\
= \text{dz. } \text{k.}$ $\text{jl. } z_4 = \text{kl. } z_5$ $= (\text{dl. } z_5) \text{ Tan B}$ $\text{dl. } z_5 = (\text{dz. } \text{k. }) \text{ Sin R Tan B}$ $\therefore \text{jl. } z_4 = (\text{dz. } \text{k. }) \text{ Sin R Tan B}$ $\therefore \text{Tan } L9 = \frac{(\text{dz. } \text{k. }) \text{ Sin R Tan B}}{(\text{dz. } \text{k. })}$ = Sin R Tan B

Tangent L10

=Tan B Sin R

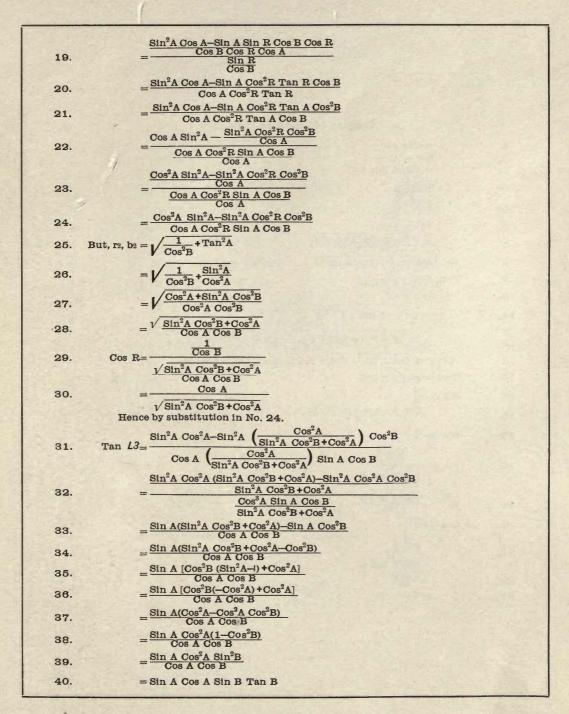
ANALYTIC PROOFS



Tangent L3

1.	Tan 13=1
2.	$=\frac{l-q}{1}$
3. 4.	j=Sin² A
4.	b2, c2=Tan A
5.	z=Cos B
6.	$= \frac{\sin^2 A}{\cos B}$
7.	ECos R
8.	$=\frac{\sin^2 A}{\cos B \cos R}$
9.	$q=(b_2, c_2) \sin R$

10.	=Tan A Sin R
11.	$= \frac{\sin A \sin R}{\cos A}$
12.	r=/-q
13.	$= \frac{\sin^2 A}{\cos B \cos R} - \frac{\sin A \sin R}{\cos A}$
14.	$(e+z) = \frac{1}{\cos B}$
15.	i=(e+z) Sin R
16.	$=\frac{1}{\cos B} \sin R$
17.	=Sin R Cos B
10	∴Tan L3 = Sin ² A Sin A Sin R Cos A Sin R
10.	Sin R Cos B



Tangent L6-Refer to Page 22.

```
a=Cos A
  1.
                        b=Cos2A
  2.
                         c=Cos A Sin A
  3.
                        d=Sin B
  4.
                        e = \frac{\cos^2 A}{\cos B}
  5.
                         f = \sqrt{d^2 + e^2}
  6.
                          = \frac{\sqrt{\sin^2 B \cos^4 A + \cos^2 B}}{\cos B \sin B}
  7.
                 Let M=\ Cos2B+Cos4A Sin2B
  8.
                                                                      (for convenience)
                Then f= M Sin B
  9.
                        h=\sqrt{c^2+f^2}
10.
                          = \sqrt{\cos^2 A \sin^2 A + \frac{\sin^2 B \cos^4 A + \cos^2 B}{\cos^2 B \sin^2 B}}
11.
                          = \frac{\sqrt{\cos^2 A \sin^2 A \cos^2 B \sin^2 B + \sin^2 B \cos^4 A + \cos^2 B}}{\cos B \sin B}
12.
                  Let P=V Cos<sup>2</sup>A Sin<sup>2</sup>A Cos<sup>2</sup>B Sin<sup>2</sup>B + Sin<sup>2</sup>B Cos<sup>4</sup>A + Cos<sup>2</sup>B
13.
               Then h=Cos B Sin B
14.
                Sin G_4 = \frac{c}{h}
15.
                          Cos A Sin A Cos B Sin B
16.
                 Sin G2=
17.
                                 Cos<sup>2</sup>A
Cos B
18.
                            M
Cos B Sin B
                          _Cos2A Sin B
19.
                                     M
                Cos G2=d
20.
21.
                            Cos B Sin B
                          =\frac{\cos B}{M}
22.
                         g=d Cos G2
23.
```

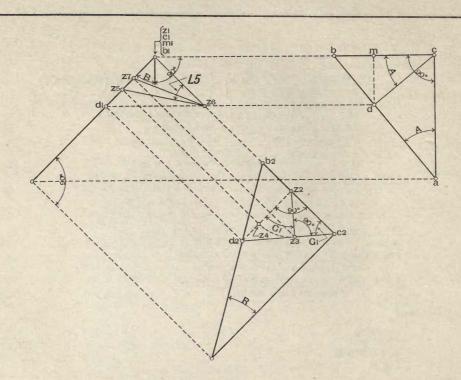
```
=\left(\frac{1}{\sin B}\right)\left(\frac{\cos B}{M}\right)
24.
                                 =\frac{\cos B}{M \sin B}
25.
                             m=g Sin G4
26.
                                  = \left(\frac{\text{Cos B}}{\text{M Sin B}}\right) \left(\frac{\text{Cos A Sin A Cos B Sin B}}{\text{P}}\right)
27.
                                  = \frac{\text{Cos A Sin A Cos}^2 B}{\text{MP}}
28.
                               k=d Sin G2
29.
                                  = \left(\frac{1}{\sin B}\right) \left(\frac{\cos^2 A \sin B}{M}\right)
30.
                                  =\frac{\cos^2 A}{M}
31.
                               s=\sqrt{k^2+m^2}
32.
                                  = \sqrt{\left(\frac{\cos^2 A}{M}\right)^2 + \left(\frac{\cos A \sin A \cos^2 B}{MP}\right)}
33.
                                  = \frac{\text{Cos A}}{\text{M P}} \sqrt{P^2 \text{Cos}^2 \text{A} + \text{Cos}^4 \text{B Sin}^2 \text{A}}
34.
                       Let N=VP2Cos2A+Cos4B Sin2A
                                                                                                (for convenience)
35.
                   Then s = \frac{N \cos A}{MP}
36.
                    Sin G_3 = \frac{m}{s}
37.
                                           Cos A Sin A Cos<sup>2</sup>B
M P
N Cos A
M P
38.
                                  = \frac{\sin A \cos^2 B}{N}
39.
                     \cos G_8 = \frac{k}{s}
40.
                                            Cos<sup>2</sup>A
41.
                                          N Cos A
                                  =P Cos A
42.
43.
                               n=g Tan (B-G2)
                                  = \left(\frac{\text{Cos B}}{\text{M Sin B}}\right) \text{Tan } (B-G_2)
44.
                                  = \frac{\text{Cos B Sin (B-G_2)}}{\text{M Sin B Cos (B-G_2)}}
45.
                                  = \frac{\text{Cos B (Sin B Cos } G_2 \text{-Cos B Sin } G_2)}{\text{M Sin B (Cos B Cos } G_2 \text{+Sin B Sin } G_2)}
46.
```

```
Cos B(Sin B Cos B - Cos B Cos A Sin B)
47.
                                     M \sin B \left( \frac{\cos^2 B}{M} + \frac{\cos^2 A \sin^2 B}{M} \right)
                            Cos B (Sin B Cos B-Cos B Cos<sup>2</sup>A Sin B)
48.
                                         M Sin B (Cos2B + Cos2A Sin2B)
                            Cos B (Cos B-Cos B Cos<sup>2</sup>A)
49.
                                  M (Cos2B + Cos2A Sin2B)
                                   Cos<sup>2</sup>B (1-Cos<sup>2</sup>A)
50.
                            M(Cos<sup>2</sup>B+Cos<sup>2</sup>A Sin<sup>2</sup>B)
                                     Cos<sup>2</sup>B Sin<sup>2</sup>A
51.
                               M (Cos<sup>2</sup>B + Cos<sup>2</sup>A Sin<sup>2</sup>B)
52.
                           p=m Tan Gs
53.
                           t=n-p
                            =n-m Tan Gs
54.
                           y=t Cos Gs
55.
56.
                            =(n-m Tan Gs) Cos Gs
                                  m
57.
                           V=Cos Gs
                          w=t Sin Gs
58.
                            =(n-m Tan Gs) Sin Gs
59.
60.
                            = m + (n-m Tan Gs) Sin Gs
61.
                     Statement for reduction
                 Tan L6 = \frac{y}{x}
62.
                                    (n-m Tan G<sub>8</sub>) (Cos G<sub>8</sub>)
                            = \frac{\frac{(n-m)^2 Tan G_8}{m} + (n-m)^2 Tan G_8}{\frac{m}{Cos} G_8} + (n-m)^2 Tan G_8} \sin G_8
63.
                            = \frac{(n-m \operatorname{Tan} G_8) \operatorname{Cos}^2 G_3}{m+(n-m \operatorname{Tan} G_8) \operatorname{Sin} G_8 \operatorname{Cos} G_8}
64.
                                         (n-m Sin G<sub>3</sub>) Cos<sup>2</sup>G<sub>3</sub>
                                m+(n-m Sin G<sub>8</sub>) Sin G<sub>8</sub> Cos G<sub>8</sub>
65.
                             = \frac{(n \cos G_3 - m \sin G_3) \cos G_3}{m + (n \cos G_3 - m \sin G_3) \sin G_3}
66.
                            = n Cos<sup>2</sup>G<sub>3</sub>-m Sin G<sub>3</sub> Cos G<sub>8</sub>
67.
                               m+n Cos G3 Sin G3-m Sin2G3
                             n Cos<sup>2</sup>G<sub>8</sub>-m Sin G<sub>3</sub> Cos G<sub>8</sub>
68.
                               m (1-Sin<sup>2</sup>G<sub>8</sub>)+n Cos G<sub>3</sub> Sin G<sub>8</sub>
                            n Cos<sup>2</sup>G<sub>8</sub>-m Sin G<sub>8</sub> Cos G<sub>8</sub>
69.
                              m Cos2Gs +n Cos Gs Sin Gs
```

ANALYTIC PROOFS

```
n Cos Gs-m Sin Gs
70.
                            m Cos Gs+n Sin Gs
                   Hence by substitution
                                                                                           Cos A Sin A Cos2B Sin A Cos2B
                                       Cos2B Sin2A
                                                                        P Cos A
                             M(Cos<sup>2</sup>B+Cos<sup>2</sup>ASin<sup>2</sup>B)
                                                                                                        MP
71.
               Tan L6=
                                                                                               Cos<sup>2</sup>B Sin<sup>2</sup>A
                                                                                                                                Sin A Cos<sup>2</sup>B
                              Cos A Sin A Cos2B
                                                                P Cos A
                                                                                    M(Cos<sup>2</sup>B+Cos<sup>2</sup>A Sin<sup>2</sup>B)
                                                                               Cos A Sin<sup>2</sup>A Cos<sup>4</sup>B
                                  P Cos<sup>2</sup>B Sin<sup>2</sup>A Cos A
                               MN(Cos2B+Cos2A Sin2B)
72.
                                                                                     Cos4B Sin8A
                                P Cos<sup>2</sup>A Sin A Cos<sup>2</sup>B
                                                                           MN(Cos2B + Cos2A Sin2B)
                           P<sup>2</sup>Cos A Cos<sup>2</sup>B Sin<sup>2</sup>A-Cos<sup>4</sup>B Sin<sup>2</sup>A Cos A (Cos<sup>2</sup>B+Cos<sup>2</sup>A Sin<sup>2</sup>B)
73.
                                P Cos<sup>2</sup>A Cos<sup>2</sup>B Sin A (Cos<sup>2</sup>B + Cos<sup>2</sup>A Sin<sup>2</sup>B) + P Cos<sup>4</sup>B Sin<sup>3</sup>A
                                     Sin<sup>2</sup>A Cos<sup>2</sup>B Cos A [P<sup>2</sup>-Cos<sup>2</sup>B (Cos<sup>2</sup>B + Cos<sup>2</sup>A Sin<sup>2</sup>B
74
                               P Sin A Cos<sup>2</sup>B [Cos<sup>2</sup>A (Cos<sup>2</sup>B + Cos<sup>2</sup>A Sin<sup>2</sup>B) + Cos B Si
                            Sin A Cos A [P<sup>2</sup>-Cos<sup>2</sup>B (Cos<sup>2</sup>B+Cos<sup>2</sup>A Sin<sup>2</sup>B)]
75.
                              P [Cos<sup>2</sup>A Cos<sup>2</sup>B + Cos<sup>4</sup>A Sin B + Cos<sup>2</sup>B Sin<sup>2</sup>A]
                            Sin A Cos A [P<sup>2</sup>-Cos<sup>2</sup>B (Cos<sup>2</sup>B+Cos<sup>2</sup>A Sin<sup>2</sup>B)]
76.
                                   P [Cos<sup>2</sup>B (Cos<sup>2</sup>A+Sin<sup>2</sup>A)+Cos<sup>4</sup>A Sin<sup>2</sup>B]
                           Sin A Cos A [P2-Cos2B(Cos2B+Cos2A Sin2B)]
77.
                                              P [Cos<sup>2</sup>B +Cos<sup>4</sup>A Sin<sup>2</sup>B]
                Cos L4=d
78.
79.
                              Sin B Cos B
                           Cos B
80.
81.
         ... P Cos L4=Cos B
                        P = \frac{\cos B}{\cos L4}
82
                       P2=Cos2A Sin2A Cos2B Sin2B+Sin2B Cos4A+Cos2B
83.
              Tan/6 = \frac{\sin A \cos A \cos L4 [\cos^2 A \sin^2 A \cos^2 B \sin^2 B + \sin^2 B \cos^4 A + \cos^2 B - \cos^4 B - \cos^4 B - \cos^2 B \sin^2 B \cos^2 A]}{\sin A \cos A \cos L4 [\cos^2 A \sin^2 A \cos^2 B \sin^2 B + \sin^2 B \cos^4 A + \cos^2 B - \cos^4 B - \cos^4 B \cos^4 A]}
84.
                                                                              Cos B [Cos2B+Cos4A Sin2B]
                           _Sin A Cos A Cos L4 [Sin<sup>2</sup>B Cos<sup>2</sup>B Cos<sup>2</sup>A (Sin<sup>2</sup>A-1)+Cos<sup>2</sup>B (1-Cos<sup>2</sup>B)+Sin<sup>2</sup>B Cos<sup>4</sup>A]
85.
                                                                      Cos B [Cos2B+Cos4A Sin2B]
                             Sin A Cos A Cos L4 [-Cos<sup>4</sup>A Sin<sup>2</sup>B Cos<sup>2</sup>B + Cos<sup>4</sup>B Sin<sup>2</sup>B + Sin<sup>2</sup>B Cos<sup>4</sup>A]
86.
                                                                         Cos B [Cos2B+Cos4A Sin2B]
                              Sin A Cos A Cos L4 [Cos<sup>4</sup> A Sin<sup>2</sup> B (1-Cos<sup>2</sup> B) + Cos<sup>2</sup> B Sin<sup>2</sup> B]
87.
                                                      Cos B (Cos2B+Cos4A Sin2B)
                              Sin A Cos A Cos L4(Cos<sup>4</sup>A Sin<sup>4</sup>B+Cos<sup>2</sup>B Sin<sup>2</sup>B)
88.
                                              Cos B (Cos<sup>2</sup>B+Cos<sup>4</sup>A Sin<sup>2</sup>B)
                              Sin A Cos A Cos L4 Sin2B (Cos4A Sin2B+Cos2B)
89.
                                               Cos B (Cos2B+Cos4A Sin2B)
                             Sin A Cos A Cos L4 Sin2B
90.
                                               Cos B
91. But, Tan L3=Sin A Cos A Sin B Tan B
                           Sin A Cos A Sin2B
92.
                                         Cos B
93.
            ... Tan L6=Cos L4 Tan L3
```

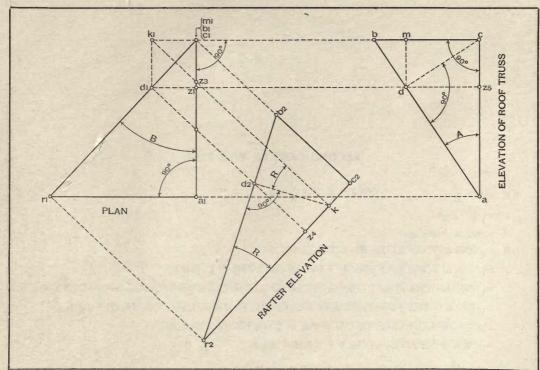
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Tangent L5

Draw d₂, z₂ 1 b₂, c₂ Pass a plane thru z₂ 1 d₂, c₂ This plane seen in plan view appears as surface z₂, z₆, z₇ Revoive this plane about z₂, z₆ to z₄ This plane then seen in plan view appears as surface z₂, z₆, z₅

PROOF FOR THE 90° USED IN STYLES C AND D



EXPLANATION FOR 90° BEND LINE ON STYLES C AND D.

Purlin Web Plane seen from Elevation of Main Roof is Line cd.

"in Plan View is Inclined Surface d1, z1, c1, k1.

Rafter Lug Plane seen in Rafter Elevation is Line d2, k.

""""""""" "Plan View is Inclined Surface d1, z3, k1.

These Two Planes produced intersect on Line d1, k1.

Hence if k1, c1 equals in length d1, z1, then will angle k1, d1, z1 be 90° in all cases.

STATEMENT OF VALUES.

ac=Unity

cd=Sin A

ad=Cos A

zi, al=Cos2A

zi, mi=Sin2A

dl, ml=Sin2A SecB

zi, di=Sin2A Tan B

dl, rl, r2, Z4=Cos2A SecB

d2, r2=Cos2A Sec B Sec R

d2, z4=d, z5=Cos A Sin A

Z4, k=Cos A Sin A Tan R

d2, b2=Sin2A SecB SecR

k, c2=Sin2A SecB-Cos A Sin A Tan R

kl, cl=(k, c2) CscB

=[Sin2A SecB-Cos A Sin A Tan R] Csc B

PROOF.

- 1. (Sin2 A Sec B-Cos A Sin A Tan R) Csc B=Sin2 A Tan B
- Sin² A Cos A Sin A Tan R

Sin P =Sin² A Tan B

3. $\frac{\sin^2 A - \cos A \sin A \cos B \operatorname{Tan} R}{\cos B \sin B} = \sin^2 A \operatorname{Tan} B$

- 4. Sin² A-Cos A Sin A Cos B Tan R=Sin² A Tan B Cos B Sin B
- 5. Sin2 A-Cos A Sin A Cos B Tan R-Sin2 A Sin2 B
- 6. Tan R=Tan A Cos B.
- 7. Sin² A-Cos A Sin A Cos B Tan A Cos B=Sin² A Sin² B.
- 8. Sin ²A-Cos A Sin A Cos B Sin A Sin B Sin B
- 9. Sin²A-Sin²A Cos²B-Sin²A Sin²B
- 10. I-Cos2B=Sin2B
- 11. |=Sin²B+Cos²B or |=| Hence Eq. 11 being true, proves Eq. 1 to be true.

SECOND CASE OF PIPE LINE

$$\frac{1}{2} \mathbf{F} = \cos \frac{\chi}{2}$$

$$\frac{1}{2} \mathbf{F} = \cos \frac{\chi}{2} \qquad \qquad \cos \chi = 2 \cos^2 \frac{\chi}{2} - 1$$

$$\mathbf{F} = \sqrt{\mathbf{C}^2 + \mathbf{E}^2}$$

$$C = Sin Al + Sin A2$$

$$E = \sqrt{(\cos A) + \cos A_2 \cos B)^2 + (\cos A_2 \sin B)^2}$$

$$F = \sqrt{(\sin A + \sin A_2)^2 + (\cos A + \cos A_2 \cos B)^2 + (\cos A_2 \sin B)^2}$$

$$= \sqrt{(\sin^2 A) + 2 \sin A} \sin A_2 + \sin^2 A_2) + (\cos^2 A) + 2 \cos A \cos A_2 \cos B + \cos^2 A_2 \cos^2 B) + (\cos^2 A_2 \sin^2 B)$$

$$=\sqrt{\sin^2 A} + \cos^2 A +$$

=
$$\sqrt{1 + \cos^2 A_2(1) + \sin^2 A_2 + 2 \cos A \cos A_2 \cos B + 2 \sin A \sin A_2}$$

$$\cos\frac{\chi}{2} = \frac{1}{2}\sqrt{2 + 2 \operatorname{Cos} A \operatorname{Cos} A_2 \operatorname{Cos} B + 2 \operatorname{Sin} A \operatorname{Sin} A_2}$$

$$\cos x = \frac{2(2 + 2 \cos Al \cos A_2 \cos B + 2 \sin Al \sin A_2)}{4} - 1$$

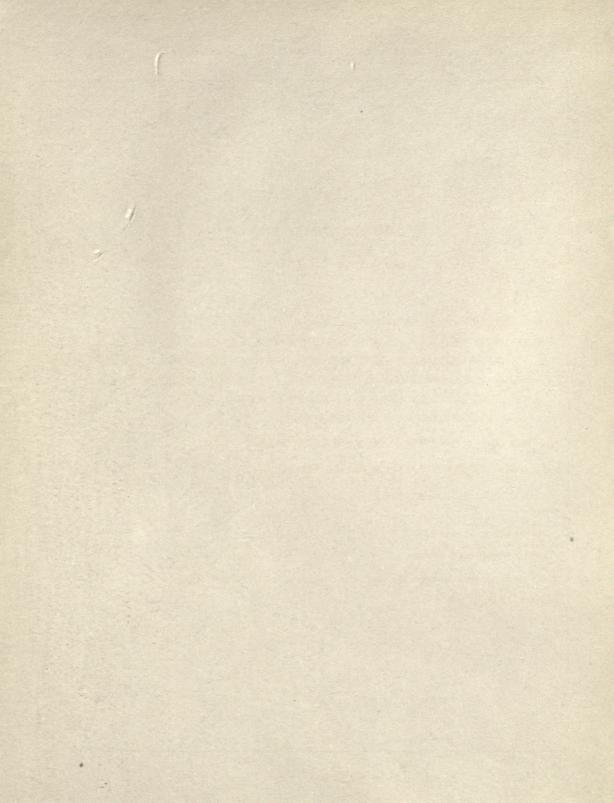
= Cos Al Cos A2 Cos B + Sin Al Sin A2

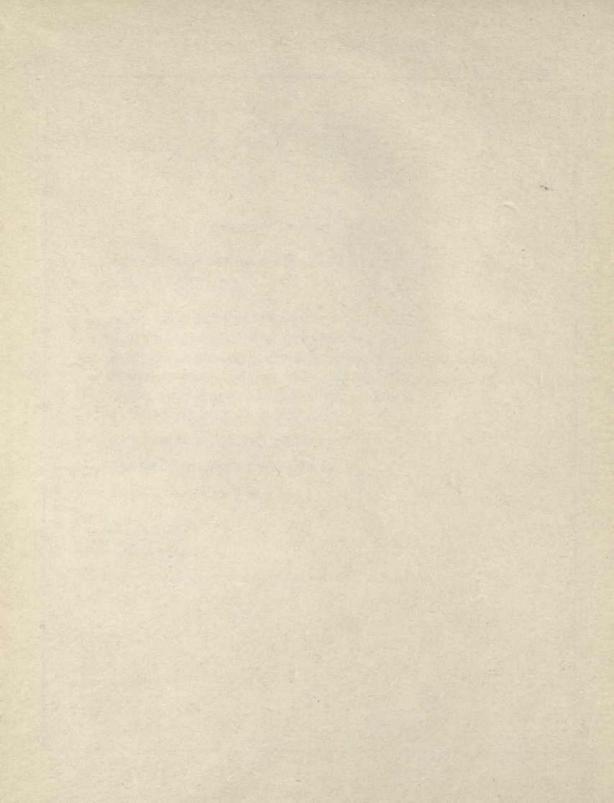
When

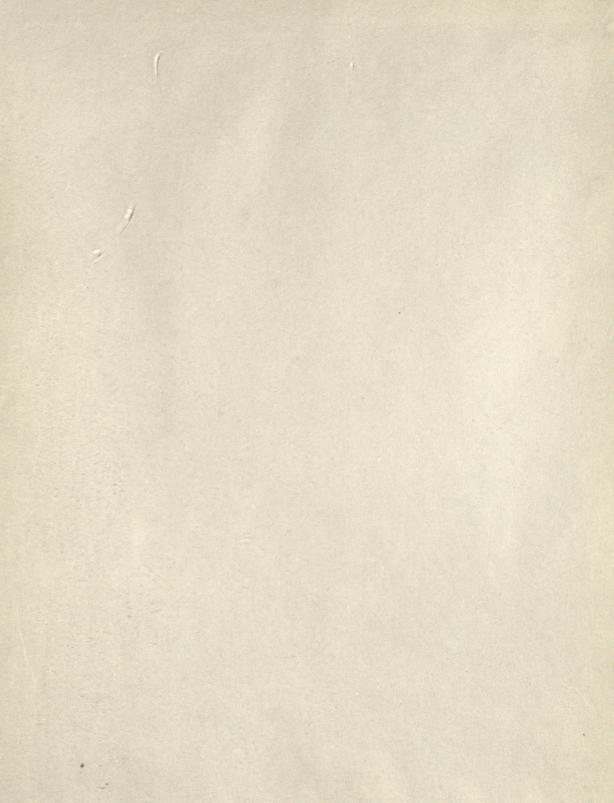
Al or $A_2 = 0$ above formula becomes Cos X = Cos A Cos B which is same as first case

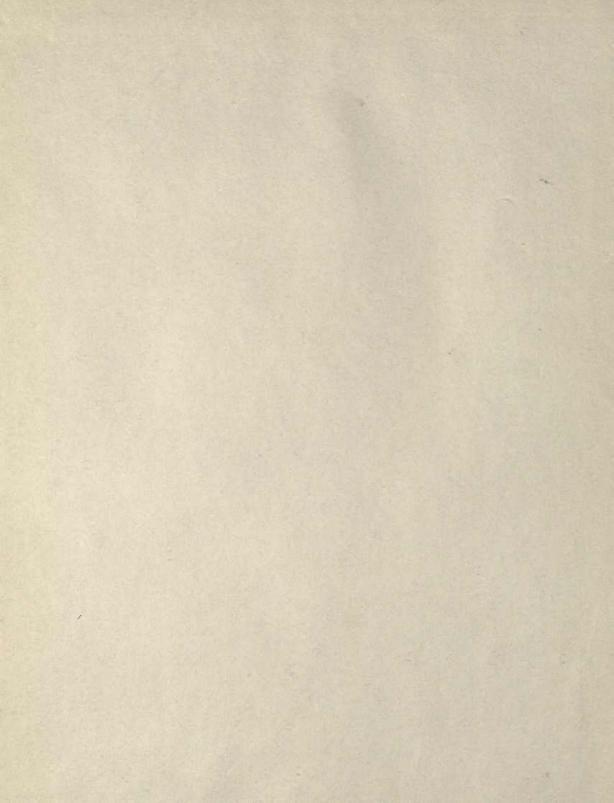
The following formula (proof omitted) was developed by Mr. C. W. L. Filkins.

$$\cos \chi = \frac{\sin A_2 \cos C_2}{\sin C_1}$$











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